HW 25 Solutions

12-89. The W8 \times 48 cantilevered beam is made of A-36 steel and is subjected to the loading shown. Determine the displacement at its end A.

Elastic Curve: The elastic curves for the concentrated load and couple moment are drawn separately as shown.

Method of Superposition: Using the table in Appendix C, the required slope and displacement are

$$\begin{split} \left(\Delta_{A}\right)_{1} &= \frac{PL_{AB}^{3}}{3EI} = \frac{1.2(16^{3})}{3EI} = \frac{1638.4 \, \text{kip} \cdot \text{ft}^{3}}{EI} \\ \left(\Delta_{C}\right)_{2} &= \frac{M_{0} \, L_{BC}^{2}}{2EI} = \frac{2(8^{2})}{2EI} = \frac{64.0 \, \text{kip} \cdot \text{ft}^{3}}{EI} \\ \left(\theta_{C}\right)_{2} &= \frac{M_{0} \, L_{BC}}{EI} = \frac{2(8)}{EI} = \frac{16.0 \, \text{kip} \cdot \text{ft}^{2}}{EI} \\ \left(\Delta_{A}\right)_{2} &= \left(\Delta_{C}\right)_{2} + \left(\theta_{C}\right)_{2} \, L_{AC} = \frac{64.0}{EI} + \frac{16.0}{EI}(8) = \frac{192 \, \text{kip} \cdot \text{ft}^{2}}{EI} \end{split}$$

The displacement at A is

$$\begin{split} & \Delta_A = (\Delta_A)_1 + (\Delta_A)_2 \\ & = \frac{1638.4}{EI} + \frac{192}{EI} \\ & = \frac{1830.4 \text{ kip} \cdot \text{ft}^3}{EI} \\ & = \frac{1830.4(1728)}{29.0(10^3)(184)} = 0.593 \text{ in.} \quad \downarrow \quad \quad \text{Ans} \end{split}$$

Ans

*12-92. The W14 \times 43 simply supported beam is made of A-36 steel and is subjected to the loading shown. Determine the slope at A and B.

$$\theta_{A} = \theta_{A_{1}} + \theta_{A_{2}}$$

$$= \frac{7wL^{3}}{384 EI} + \frac{ML}{6 EI}$$

$$= \frac{7(2)(240^{3})}{384 EI} + \frac{40(12)(240)}{6EI} = \frac{61,200}{29(10^{3})(428)}$$

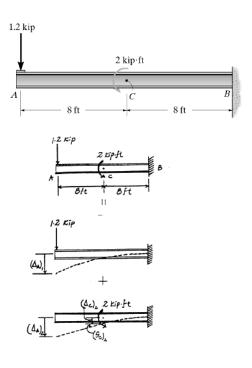
$$= 0.00493 \text{ rad} = 0.283^{\circ} \qquad \text{Ans}$$

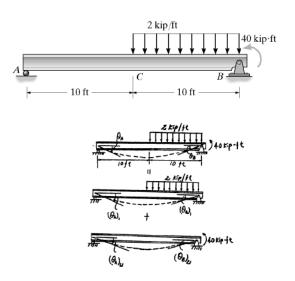
$$\theta_{B} = \theta_{B_{1}} + \theta_{B_{2}}$$

$$= \frac{3wL^{3}}{128 EI} + \frac{ML}{3 EI}$$

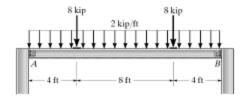
$$= \frac{\frac{3(2)}{12}(240^{3})}{128 EI} + \frac{40(12)(240)}{3EI} = \frac{92,400}{29(10^{3})(428)}$$

$$= 0.007444 \text{ rad} = 0.427^{\circ} \qquad \text{Ans}$$





12-95. The simply supported beam carries a uniform load of 2 kip/ft. Code restrictions, due to a plaster ceiling, require the maximum deflection not to exceed 1/360 of the span length. Select the lightest-weight A-36 steel wideflange beam from Appendix B that will satisfy this requirement and safely support the load. The allowable bending stress is $\sigma_{\text{allow}} = 24 \text{ ksi}$ and the allowable shear stress is $\tau_{\text{allow}} = 14 \text{ ksi}$. Assume A is a pin and B a roller support.



*M*_{max} = 96 kip ⋅ ft

Strength criterion:

$$\sigma_{\text{allow}} = \frac{M}{S_{\text{mg'd}}}$$

$$24 = \frac{96(12)}{S_{req'd}}$$

$$S_{\text{reg'd}} = 48 \text{ in}^3$$

2 hip 2 hip/fd. 2 hip/fd. 2 hip/ 2 hip/fd. 2 hip. 2 hip/ 2 hip/fd. 2 hip/ 2 hip/fd. 2 hip/ 2 hip/fd. 2 hip/ 2 hip/fd.

ned.q = 40 m

Choose W14 x 34, $S = 48.6 \text{ in}^3$, $t_w = 0.285 \text{ in.}$, d = 13.98 in., $I = 340 \text{ in}^4$

$$\tau_{allow} = \frac{V}{A_{mab}}$$

$$14 \ge \frac{24}{(13.98)(0.285)} = 6.02 \text{ ksi}$$
 OK

Deflection criterion;

Maximum is at center.

$$\begin{split} \nu_{\max} &= \frac{5wL^4}{384EI} + (2)\frac{P(4)(8)}{6EI(16)}[(16)^2 - (4)^2 - (8)^2)](12)^3 \\ &= [\frac{5(2)(16)^4}{384EI} + \frac{117.33(8)}{EI}](12)^3 \\ &= \frac{4.571(10^6)}{29(10^4)(340)} = 0.000464 \text{ in.} < \frac{1}{360}(16)(12) = 0.533 \text{ in.} \quad \text{OK} \end{split}$$

Use W14 x34 Ans

13-7. The rod is made from a 1-in.-diameter steel rod. Determine the critical buckling load if the ends are roller supported. $E_{\rm st} = 29(10^3)$ ksi, $\sigma_Y = 50$ ksi.

20 in.

Critical Buckling Load: $I = \frac{\pi}{4} (0.5^4) = 0.015625 \pi \text{ in}^4$ and K = 1 for roller supported ends column. Applying Euler's formula,

$$P_{cr} = \frac{\pi^2 EI}{(KL)^2}$$

$$= \frac{\pi^2 (29) (10^3) (0.015625\pi)}{[1(20)]^2}$$

$$= 35.12 \text{ kip} = 35.1 \text{ kip} \qquad \text{Ans}$$

Critical Stress: Euler's formula is only valid if $\sigma_{cr} < \sigma_{\gamma}$.

$$\sigma_{\rm cr} = \frac{P_{\rm cr}}{A} = \frac{35.12}{\frac{\pi}{4}(1^2)} = 44.72 \text{ ksi} < \sigma_{\gamma} = 50 \text{ ksi } (O.K!)$$

*13-8. An A-36 steel column has a length of 5 m and is fixed at both ends. If the cross-sectional area has the dimensions shown, determine the critical load.

$$I = \frac{1}{12}(0.1)(0.05^{3}) - \frac{1}{12}(0.08)(0.03^{3}) = 0.86167 (10^{-6}) \text{ m}^{4}$$

$$P_{cr} = \frac{\pi^{2}EI}{(KL)^{2}} = \frac{\pi^{2}(200)(10^{9})(0.86167) (10^{-6})}{[(0.5)(5)]^{2}}$$

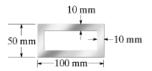
$$= 272 138 \text{ N}$$

$$= 272 \text{ kN} \quad \text{Ans}$$

$$\sigma_{cr} = \frac{P_{cr}}{A}; \qquad A = (0.1)(0.05) - (0.08)(0.03) = 2.6 (10^{-3}) \text{ m}^{2}$$

$$= \frac{272 138}{2.6 (10^{-3})} = 105 \text{ MPa} < \sigma_{\gamma}$$

Therefore, Euler's formula is valid.



13-9. An A-36 steel column has a length of 15 ft and is pinned at both ends. If the cross-sectional area has the dimensions shown, determine the critical load.

$$I_x = \frac{1}{12}(8)(7^3) - \frac{1}{12}(7.5)(6^3) = 93.67 \text{ in}^4$$

$$I_y = 2\left(\frac{1}{12}\right)(0.5)(8^3) + \frac{1}{12}(6)(0.5^3) = 42.729 \text{ in}^4 \text{ (controls)}$$

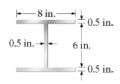
$$P_{cr} = \frac{\pi^2 EI}{(KL)^2} = \frac{\pi^2 (29)(10^3)(42.729)}{[(1.0)(15)(12)]^2}$$

$$= 377 \text{ kip} \qquad \text{Ans}$$

Check:

$$A = (2)(8)(0.5) + 6(0.5) = 11 \text{ in}^2$$

 $\sigma_{cr} = \frac{P_{cr}}{A} = \frac{377}{11} = 34.3 \text{ ksi} < \sigma_Y$



13–14. The W8 \times 67 is used as a structural A-36 steel column that can be assumed fixed at its base and pinned at its top. Determine the largest axial force P that can be applied without causing it to buckle.

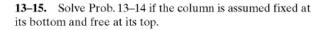
Critical Buckling Load: $I_y = 88.6 \text{ in}^4$ for a W8×67 wide flange section and K = 0.7 for one end fixed and the other end pinned. Applying Euler's formula,

$$P_{cr} = \frac{\pi^2 EI}{(KL)^2}$$

$$= \frac{\pi^2 (29) (10^3) (88.6)}{[0.7(25) (12)]^2}$$
= 575 kip Ans

Critical Stress: Euler's formula is only valid if $\sigma_{cr} < \sigma_{\gamma}$. $A = 19.7 \text{ in}^2 \text{ for a W8} \times 67 \text{ wide flange section.}$

$$\sigma_{\rm cr} = \frac{P_{\rm cr}}{A} = \frac{575.03}{19.7} = 29.19 \text{ ksi} < \sigma_{\gamma} = 36 \text{ ksi } (O.K!)$$



Critical Buckling Load: $I_y = 88.6 \text{ in}^4 \text{ for a W8} \times 67 \text{ wide}$ flange section and K = 2 for one end fixed and the other end free. Applying Euler's formula,

$$P_{cr} = \frac{\pi^2 EI}{(KL)^2}$$

$$= \frac{\pi^2 (29) (10^3) (88.6)}{[2(25) (12)]^2}$$

$$= 70.4 \text{ kip} \qquad \text{Ans}$$

Critical Stress: Euler's formula is only valid if $\sigma_{\rm cr} < \sigma_{\gamma}$. $A = 19.7 \, {\rm in}^2$ for a W8×67 wide flange section.

$$\sigma_{cr} = \frac{P_{cr}}{A} = \frac{70.44}{19.7} = 3.58 \text{ ksi} < \sigma_{\gamma} = 36 \text{ ksi } (O.K!)$$



