



Introduction to Heat Transfer in Soils and Other Materials

ME 7710
Spring 2013

Surface/Skin Temperature

- T_s - The temperature at the air-soil interface. For an “ideal” surface which varies in time in response to energy fluxes at the surface
 - Depends on:
 - *Radiation Balance*
 - *Surface exchange processes*
 - *Vegetative cover*
 - *Thermal properties of the subsurface*
 - Difficult to Measure (very large temperature gradients near the surface both in the air & soil)
 - Extrapolate air/soil temps
 - Radiometer – uses $R_L \uparrow \sim -\epsilon\sigma T_s^4$

Diurnal Soil & Air Temperatures

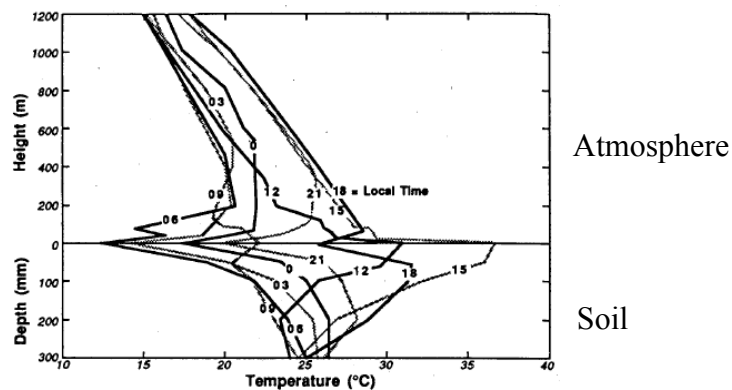


Fig. 7.17 Three day average of temperature profiles at indicated hours for the Koorin field program, days 7-9. Note the scale difference between height and depth. (After Lettau, personal communication).

Fig from Stull, 1988
An Introduction to Boundary Layer Meteorology

Surface/Skin Temperature

- Diurnal Range
 - In dry desert ~ 40-50 °C
 - Surface & subsurface moisture moderate range
 - Increased evaporation from the surface
 - Increased heat capacity (c) & conductivity of the soil (k)
 - Wet soils may dry changing the temperature response
 - Vegetation moderates diurnal range
 - Intercepts incoming solar – lower surface temps during the day
 - Intercepts outgoing longwave
 - Enhanced latent heat flux due to evapotranspiration (ET)
 - Increased Turbulence

Sub-surface Soil Temperature

- Much easier to measure – thermocouple
- Amplitude of the temperature fluctuations decrease exponentially with depth
- Depends on –
 - Latitude
 - Time of year
 - Net radiation
 - Soil texture (porosity) and moisture content
 - Ground cover
 - Surface weather conditions

Thermal Properties of Soil

- Specific Heat – c ($\text{J kg}^{-1} \text{K}^{-1}$) – the amount of heat absorbed by a material to raise the temperature of a unit mass of material by 1°
- Thermal Conductivity – k ($\text{W m}^{-1} \text{K}^{-1}$) – material property; the ability of a material to conduct heat
- Thermal Diffusivity – α_h ($\text{m}^2 \text{s}^{-1}$) Ratio of thermal conductivity to heat capacity

1D Thermal Conduction

Fourier's conduction law

$$\frac{\partial}{\partial t}(\rho c T) = -\frac{\partial H_G}{\partial z}$$

$$H_G = -k \frac{\partial T}{\partial z}$$

$$\frac{\partial}{\partial t}(\rho c T) = k \frac{\partial^2 T}{\partial z^2}$$

$$\alpha_h = \frac{k}{\rho c} = \frac{k}{C}$$

Soil heat capacity

$$\frac{\partial T}{\partial t} = \alpha_h \frac{\partial^2 T}{\partial z^2}$$

Solutions

- Analytical – multiple methods
- Numerical (e.g.) – e.g. finite difference
- Force Restore – 2 Layer Slab Model (See Stull Ch. 7, Backadar, 1976)

Diurnal & Annual Soil Temperature Temporal Variability

Diurnal Wave

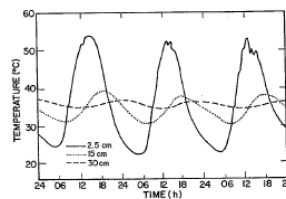


Figure 4.1 Observed diurnal course of subsurface soil temperatures at various depths in a sandy loam soil with bare surface. [From Deacon (1969); after West (1952).]

Annual Wave

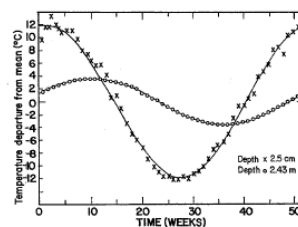


Figure 4.2 Annual temperature waves in the weekly averaged subsurface soil temperatures at two depths in a sandy loam soil. Fitted solid curves are sine waves. [From Deacon (1969); after West (1952).]

Soil Heat Transfer

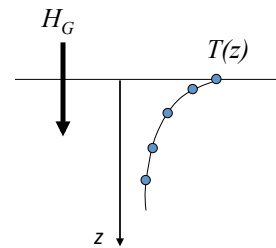
- 1D Thermal Conduction

$$\int_{z=0}^{z=D} \left\{ \frac{\partial}{\partial t} (CT) = -\frac{\partial H}{\partial z} \right\} dz$$

$$H(z=0) - H(z=D) = \int_{z=0}^{z=D} \frac{\partial}{\partial t} (CT) dz$$

$$H_G = H_D + \int_{z=0}^{z=D} \frac{\partial}{\partial t} (CT) dz$$

Surface Heat Flux \nearrow
 Reference depth \nearrow
 Storage \nwarrow



Governing Parameters

- Thermal conductivity - k
- Heat Capacity - C_s
- Thermal Diffusivity - α (sometime κ)
- Thermal Admittance - μ

Governing Parameters

- Thermal conductivity – k ($\text{W m}^{-1} \text{K}^{-1}$)
 - Def. - the ability of a material to conduct heat
 - Depends on:
 - Soil particles
 - Porosity
 - Moisture content

Governing Parameters

- Heat Capacity – $C_s = \rho c$ ($\text{J m}^{-3} \text{K}^{-1}$)
 - c specific heat of the soil ($\text{J kg}^{-1} \text{K}^{-1}$)
 - Relates to the ability of a material to store heat
 - Def. The amount of heat (J) necessary to increase a unit volume (m^3) of a substance by 1 K.
 - Water ($\sim 5 \text{ J m}^{-3} \text{K}^{-1}$) has a very high heat capacity, air is quite low
 - Depends on porosity, mineral content, organic content, air, etc.

Governing Parameters

- Thermal Diffusivity – $\alpha = k/C_s$ ($\text{m}^2 \text{s}^{-1}$)
 - Controls the speed at which temperature waves move through the soil & the depth of thermal influence of an active surface
 - Water ($\sim 5 \times 10^6 \text{ J m}^{-3} \text{ K}^{-1}$) has a very high heat capacity, air is quite low

Let's Look at example Data from Sage Brush at DPG

Governing Parameters

- Thermal Admittance – Surface Property (not a “soil property”)
- $\mu = (kC_s)^{1/2}$ ($\text{J m}^{-2} \text{s}^{-1/2} \text{K}^{-1}$)
 - Def. The ability of a surface to accept or release heat
 - High μ – metals
 - low μ – wood
 - High μ materials feel cooler to the touch even though they have the same surface temperature

Typical Values

Table 2.1 Thermal properties of natural materials

| Material | Remarks | ρ Density (kg m^{-3} $\times 10^3$) | c Specific heat ($\text{J kg}^{-1} \text{K}^{-1}$ $\times 10^3$) | C Heat capacity ($\text{J m}^{-3} \text{K}^{-1}$ $\times 10^6$) | k Thermal conductivity ($\text{W m}^{-1} \text{K}^{-1}$) | κ Thermal diffusivity ($\text{m}^2 \text{s}^{-1}$ $\times 10^{-6}$) | μ Thermal admittance ($\text{J m}^{-2} \text{s}^{-1/2} \text{K}^{-1}$) |
|-----------------------------------|-------------|--|--|---|---|--|---|
| Sandy soil (40% pore space) | Dry | 1.60 | 0.80 | 1.28 | 0.30 | 0.24 | 620 |
| | Saturated | 2.00 | 1.48 | 2.96 | 2.20 | 0.74 | 2550 |
| Clay soil (40% pore space) | Dry | 1.60 | 0.89 | 1.42 | 0.25 | 0.18 | 600 |
| | Saturated | 2.00 | 1.55 | 3.10 | 1.58 | 0.51 | 2210 |
| Peat soil (80% pore space) | Dry | 0.30 | 1.92 | 0.58 | 0.06 | 0.10 | 190 |
| | Saturated | 1.10 | 3.65 | 4.02 | 0.50 | 0.12 | 1420 |
| Snow | Fresh | 0.10 | 2.09 | 0.21 | 0.08 | 0.10 | 130 |
| | Old | 0.48 | 2.09 | 0.84 | 0.42 | 0.40 | 595 |
| Ice | 0°C, pure | 0.92 | 2.10 | 1.93 | 2.24 | 1.16 | 2080 |
| Water* | 4°C, still | 1.00 | 4.18 | 4.18 | 0.57 | 0.14 | 1545 |
| Air* | 10°C, still | 0.0012 | 1.01 | 0.0012 | 0.025 | 21.50 | 5 |
| | Turbulent | 0.0012 | 1.01 | 0.0012 | ~125 | ~ 10×10^6 | 390 |

* Properties depend on temperature, see Appendix A3.
Sources: van Wijk and de Vries (1963), List (1966).

From Oke, 1988

Effect of Soil Moisture on Thermal Properties

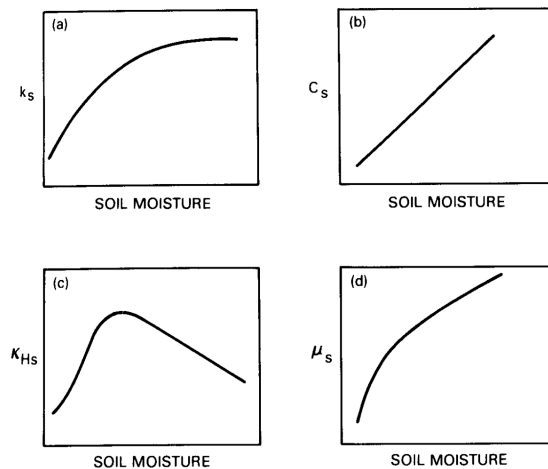
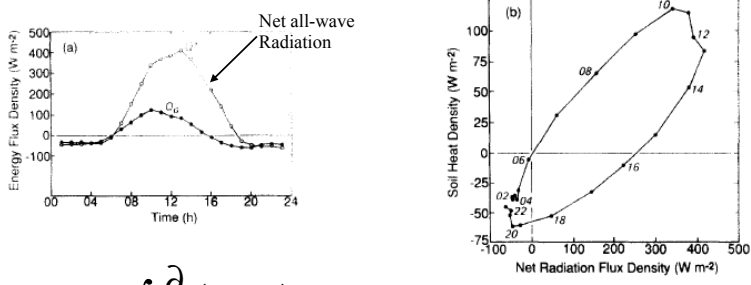


Figure 2.5 Relationship between soil moisture content: (a) thermal conductivity, (b) heat capacity, (c) thermal diffusivity and (d) thermal admittance for most soils.

From Oke, 1988

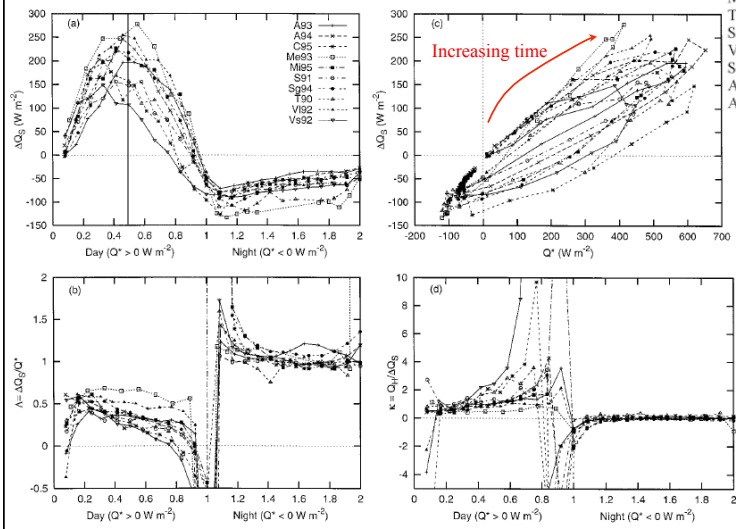
Hysteresis



$$\Delta H_s = \int \frac{\partial}{\partial t} (\rho C T) dz$$

Fig. 1. (a) Time series and (b) hysteresis loop relations between soil heat flux and net all-wave radiation for short grass near St Louis, MO calculated from the data of Doll *et al.* (1985) for a single day. Best fit statistics give the equation: $Q_G = 0.32Q^* + 0.54(\partial Q^* / \partial t) - 27.4$.

Urban Areas



| Site | Code |
|---------------------|------|
| Mexico City, D.F. | Me93 |
| Vancouver, BC | V192 |
| Chicago, IL | C95 |
| Miami, FL | Mi95 |
| Tucson, AZ | T90 |
| San Gabriel, LA, CA | Sg94 |
| Vancouver, BC* | Vs92 |
| Sacramento, CA | S91 |
| Arcadia, LA, CA | A94 |
| Arcadia, LA, CA | A93 |

More Energy is transferred to the "urban fabric" in the morning - Asymmetry

FIG. 1. Mean diurnal patterns of observed (a) ΔQ_G ($W m^{-2}$), (b) $\Delta Q_G/Q^*$, (c) ΔQ_G vs Q^* , and (d) $Q_G/\Delta Q_G$ for each of the datasets (see details in Table 1).

Grimmond & Oke 1990