

Boundary Layers in a Pressure Gradient

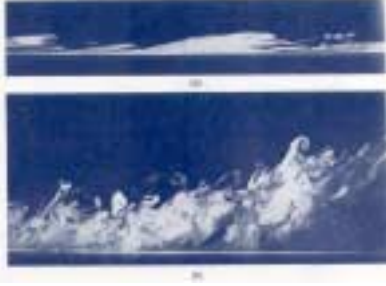


Figure from
Potter & Wiggert 1997

External Flows

Skin Friction vs. Pressure Drag

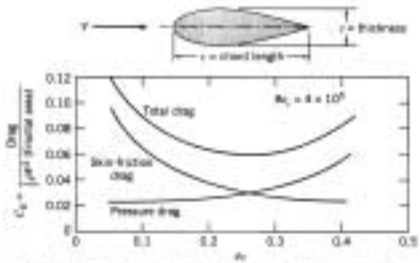
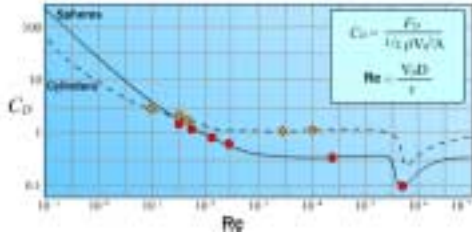


Fig. 8.14 Drag coefficient on a streamlined airfoil as a function of thickness ratio, showing contributions of skin friction and pressure to total drag (TR).

Figure from Fox et al. 2004

Drag on Sphere & Cylinders

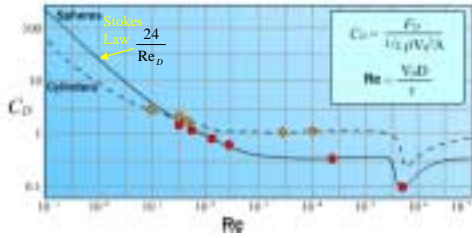
Cylinders & Spheres: Prior to separation both components of drag can be significant.



See MM Video

Drag

Cylinders & Spheres: Prior to separation both components of drag can be significant.



See MM Video

Drag

Cylinders & Spheres: Prior to separation both components of drag can be significant.

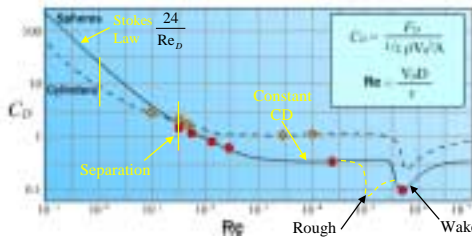


Figure From Cambridge Media-media CD

Sphere Flow Separation

Can not determine Separation point analytically (as it may move dynamically), we must use experiments or numerical solutions to N-S equations

See MM Video

Method of Drag Reduction

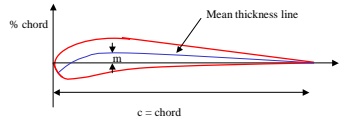
1. Streamlining – reduce pressure drag - reduce regions of $dp/dx > 0$ (either in size or magnitude) – prevent separation
 - i. Add fairings – prevent buffeting & vortex shedding
 - ii. Contour leading or Trailing edges – for struts, columns, etc
 - iii. For Airfoils – move position of maximum thickness rearward (recall $dp/dx < 0$ inhibits separation & $dp/dx > 0$ promotes separation)

2. Reducing Friction Drag
 1. Oil pipeline – introduce a thin film of water around edge of pipe – oil rides over low viscosity water – reduces drag ~60%
 2. Vee-Groove micro Riblets – stream oriented and are effective at reducing drag ~8%
 3. Large Eddy Breakup Devices – reduces local friction ~10%
3. Biological Drag Reduction – trees & leaves

Airfoils - Symmetric

Symmetric Airfoils have no lift at $\alpha = 0$

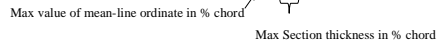
Airfoils - Cambered



Cambered Airfoils have lift at $\alpha = 0$

Naming Convention:

NACA 4-digit Series: Example NACA 0012



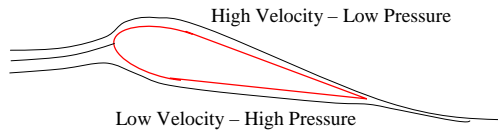
Lift Force

- The purpose of an airfoil is to generate a Force normal to the approach velocity - Lift Force - F_L

$$C_L = \frac{F_L}{\frac{1}{2} \rho U_\infty^2 A_p}$$

- Lift is generated by an imbalance in pressure along the upper and lower surfaces

$$F_L = \int (p \sin \alpha) dS$$



Lift Force - Circulation - Γ

Path Dependant

$$\frac{F_L}{L} = -\rho U_\infty \Gamma$$

$$\Gamma = \oint_C \vec{V} \cdot d\vec{l} = \int_A (\vec{\omega} \cdot \hat{n}) dA$$

$$d\vec{l} = dx\hat{i} + dy\hat{j} + dz\hat{k}$$

Example Problems:

